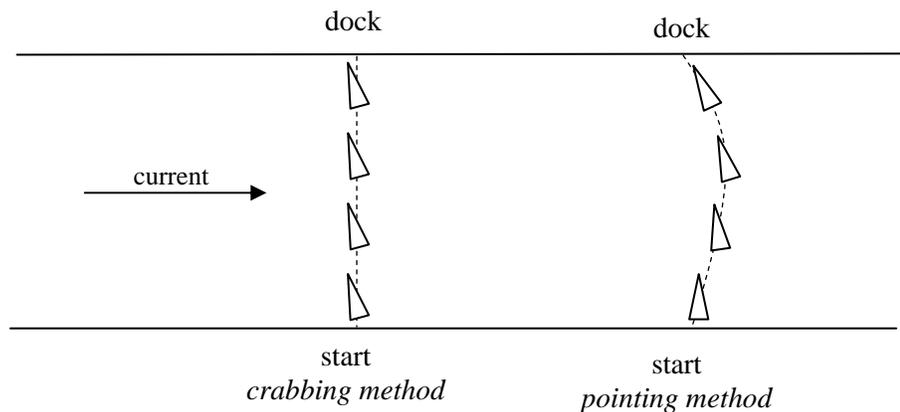


boat time

Suppose you are anchored near the shore of a channel in which there is steady current, and you are going to run your (motor)boat at constant throttle to a dock directly across the channel on the opposite shore. There are two ways one might steer the boat to the dock:

- *the crabbing method*: steer a steady course with the nose of the boat pointed somewhat upstream, so the boat maintains a fixed orientation and crabs in a straight line across the channel
- *the pointing method*: keep the nose of the boat pointed directly at the dock



Which method gets the boat to the dock faster, and by how much? (Assume the boat runs at a constant speed relative to the water, which is faster than the speed of the current relative to the shore.)

Solution by Riccardo Borghi

We denote by v_c the current speed and by v_b the boat speed with respect to the water. The speed, say v , of the boat with respect to the dock will then be given by

$$v = v_c + v_b \quad (1)$$

Moreover, we introduce the ratio, say η , between the modula of v_c and v_b as

$$\eta = \frac{v_b}{v_c} \quad (2)$$

which will be supposed to be greater than one. Finally, we denote by D the distance between the starting point, say P , and the arrival point, say O . We will analyze separately the two methods proposed to get the dock.

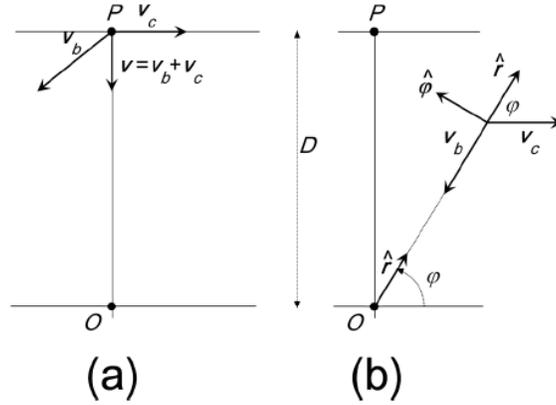


Fig. 1

- *Crabbing method.* The situation is depicted in Fig. 1a. In this case the speed v is a constant vector directed along the line connecting the points P and O . Its modulus v is then simply given by Pitagora's theorem and the navigation time, say T_1 , turns out to be

$$T_1 = \frac{D}{v_c} \frac{1}{\sqrt{\eta^2 - 1}} \quad (3)$$

- *Pointing method.* To find the navigation time, say T_2 , we will first determine the boat trajectory for a given η . To find it, we use a *polar* reference frame, say (r, φ) , having the origin at the arrival point O . The situation is depicted in Fig. 1b. With respect to such a reference frame, the boat speed v will be expressed as

$$\mathbf{v} = \dot{r} \hat{\mathbf{r}} + r \dot{\varphi} \hat{\boldsymbol{\varphi}} \quad (4)$$

As far as the r.h.s. of Eq. (1) is concerned, always from Fig. 1b we have

$$\mathbf{v}_b = -v_b \hat{\mathbf{r}} \quad (5a)$$

$$\mathbf{v}_c = v_c \cos \varphi \hat{\mathbf{r}} - v_c \sin \varphi \hat{\boldsymbol{\varphi}} \quad (5b)$$

so that we have to solve the following system:

$$\dot{r} = v_c \cos \varphi - v_b \quad (6a)$$

$$r \dot{\varphi} = -v_c \sin \varphi \quad (6b)$$

with the initial conditions $r(0)=D$ and $\varphi(0)=\pi/2$. The boat trajectory can be obtained by employing a trick used by A. Sommerfeld to determine the form of Keplerian orbits.¹ In particular, on dividing side by side Eqs. (6a) and (6b), we have

$$\frac{1}{r} \frac{dr}{d\varphi} = \frac{\eta - \cos \varphi}{\sin \varphi} \quad (7)$$

that can be solved at once simply by separating variables r and φ .

¹ A. Sommerfeld, *Lectures on Theoretical Physics. I. Mechanics* (Academic Press, 1970)

Note that the boat trajectory corresponds to the boundary condition $r(\pi/2)=D$, which gives

$$\int_D^r \frac{dr}{r} = \int_{\pi/2}^{\varphi} \frac{\eta - \cos \varphi}{\sin \varphi} d\varphi \quad (8)$$

Both integrals are expressed via elementary functions and give²

$$r(\varphi) = D \frac{\left(\tan \frac{\varphi}{2}\right)^\eta}{\sin \varphi} \quad (9)$$

To find T_2 it is now sufficient to substitute from Eq. (9) into Eq. (6b), to separate variables φ and t and to integrate side by side. We have, on taking into account that $\varphi(0)=\pi/2$ and $\varphi(T_2)=0$,

$$T_2 = \frac{D}{v_c} \int_0^{\pi/2} \frac{\left(\tan \frac{\varphi}{2}\right)^\eta}{\sin^2 \varphi} d\varphi \quad (10)$$

On evaluating the last integral³ we have

$$T_2 = \frac{D}{v_c} \frac{\eta}{\eta^2 - 1} \quad (11)$$

which, together with Eq. (3), gives at once

$$\frac{T_2}{T_1} = \frac{\eta}{\sqrt{\eta^2 - 1}} = \frac{1}{\sqrt{1 - \frac{v_c^2}{v_b^2}}} \quad (14)$$

² The following indefinite integral should be taken into account:

$$\int \frac{\eta - \cos \varphi}{\sin \varphi} d\varphi = \eta \log \tan \frac{\varphi}{2} - \log \sin \varphi$$

³ We have

$$\int_0^{\pi/2} \frac{\left(\tan \frac{\varphi}{2}\right)^\eta}{\sin^2 \varphi} d\varphi = \frac{1}{2} \int_0^{\pi/2} \frac{\left(\tan \frac{\varphi}{2}\right)^\eta}{\sin^2 \frac{\varphi}{2}} \frac{d\varphi}{2 \cos^2 \frac{\varphi}{2}}$$

that, on making the substitution $u=\tan \varphi/2$ and on expressing sine and cosine via tangent, takes on the form

$$\frac{1}{2} \int_0^1 u^{\eta-2} (1+u^2) du = \frac{1}{2} \int_0^1 (u^{\eta-2} + u^\eta) du = \frac{1}{2} \left(\frac{1}{\eta-1} + \frac{1}{\eta+1} \right) = \frac{\eta}{\eta^2-1}$$